

CCC Annual Report

UIUC, August 20, 2014

Modeling SEN Preheating

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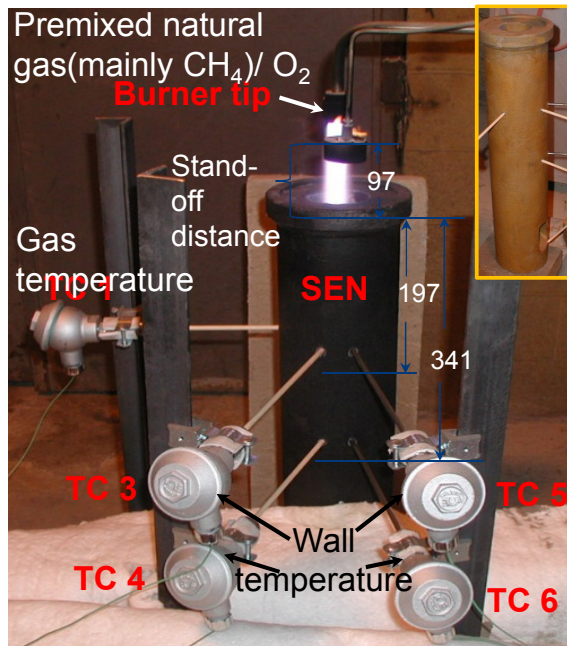
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Objectives

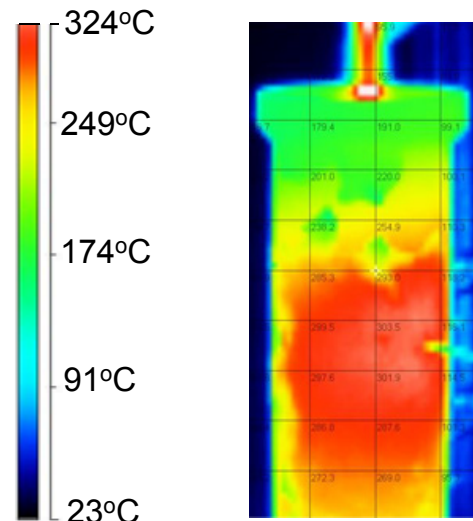
- Develop an accurate preheating model to optimize preheating process:
 - Fuel composition;
 - Preheating time;
 - Torch configuration;
 - Insulation;
 - Refractory conductivity.
- Obtain **air entrainment**, flow and temperature distributions from combustion model.
- Evaluate Flame Temperature Model (in spread-sheet).

Preheating experiment setup^[1]

Two-port SEN

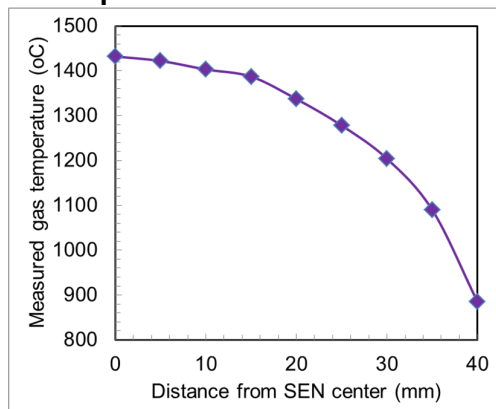


Infra-red photo of SEN outside wall



Measurements^[2] (for model validation)

1. Gas temperature 197mm below SEN top



2. Wall temperature (transient are not listed here.)

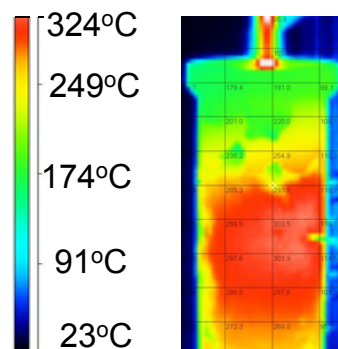
Thermocouple	TC3	TC4	TC5	TC6
X^* (mm)	394	538	394	538
Y^* (mm)	48	48	69	69
Temp. (°C)	584	554	453	397

X: Distance from top air inlet;
Y: Distance from SEN centerline.

3. The shape of flame

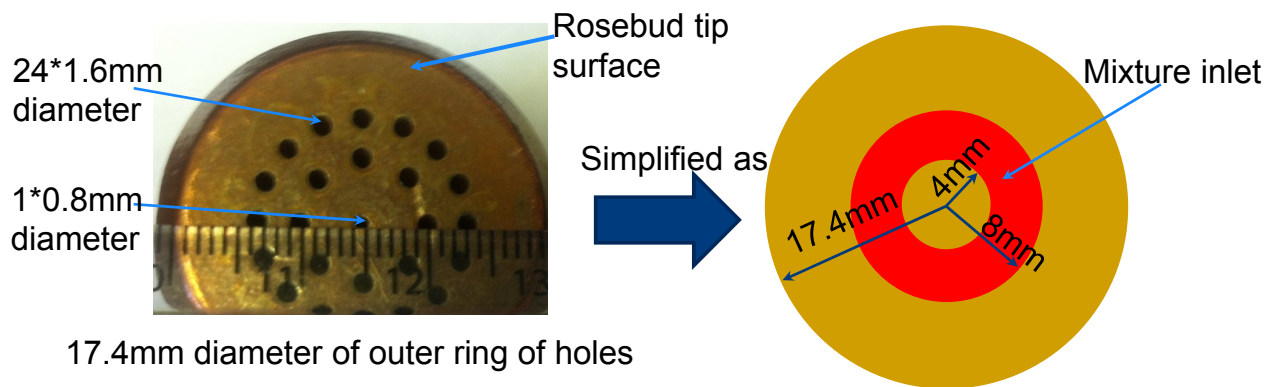


4. SEN outside wall temperature

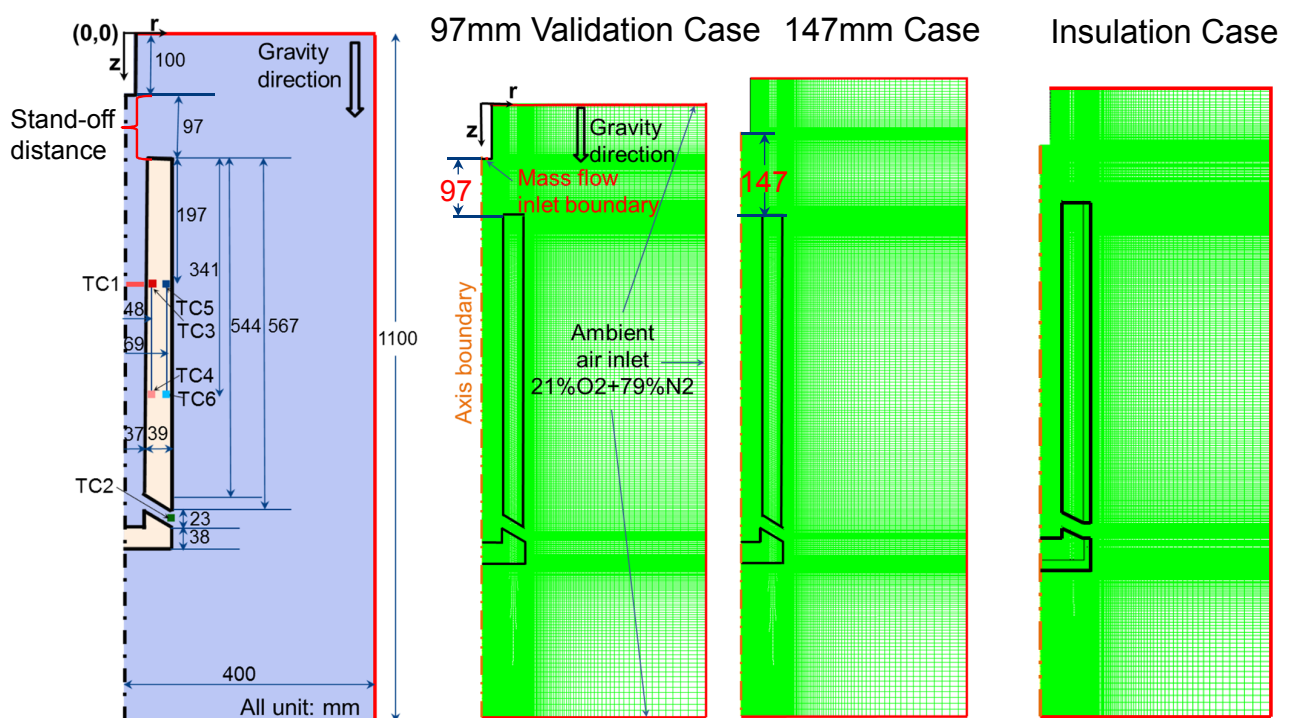


Thermal – Flow Model

- FLUENT simulation is 2D axisymmetric.
 - The two-port SEN is simplified as a ring shaped port with the same exit area.
- The burner tip is assumed as annular shape with 3× bigger area.
 - To avoid supersonic and mesh refinement at burner tip, accounting for gas expansion.



Model geometry and mesh



88843 quadrilateral cells total

1-mm coating layer with 4 cells through thickness

Material Properties

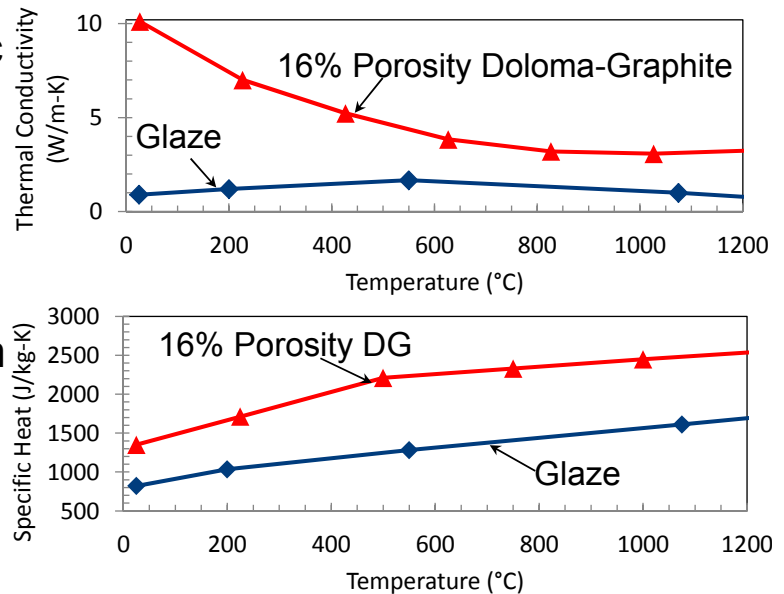
- Flow

- ✓ Species thermodynamic properties: thermo.db

- ✓ Gas average [3] thermal conductivity 2.7006 W/mK

- ✓ viscosity 9.32×10^{-5} kg/m

- SEN [1,4,5]



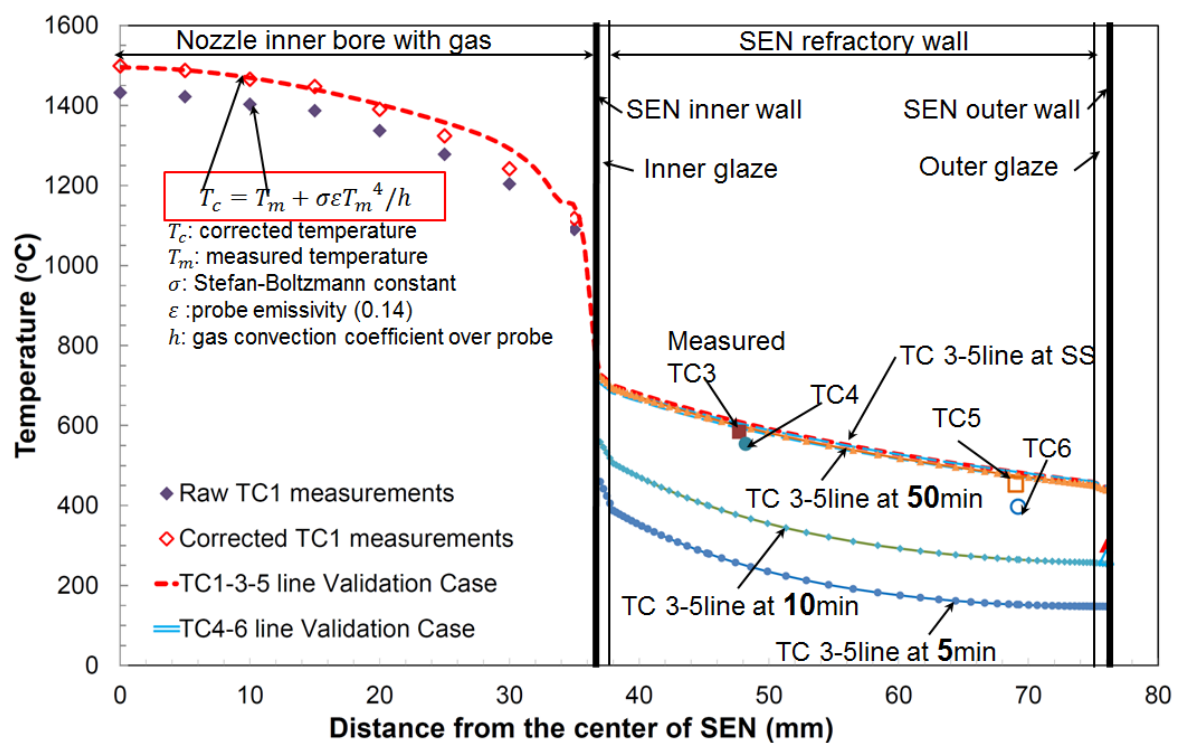
Key features--combustion

- Non-premixed species model.
- Fuel inlet: perfectly mixed CH_4 and O_2 in 1:2 mole ratio in a total mass flow rate of 3.8 g/s^[2].
- Ambient air entrainment.
- Non-adiabatic energy treatment.
- GRI-Mech 3.0^[6] natural gas combustion mechanism, contains **325** reactions and **53** species.

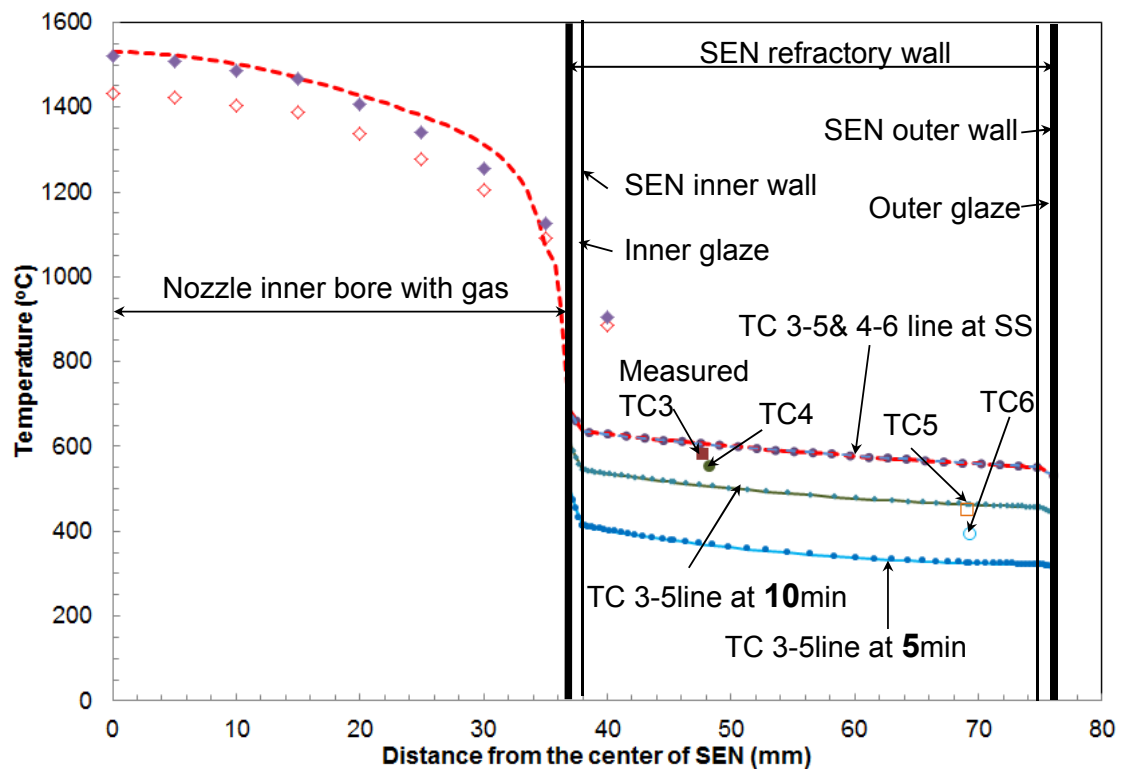
Model validation

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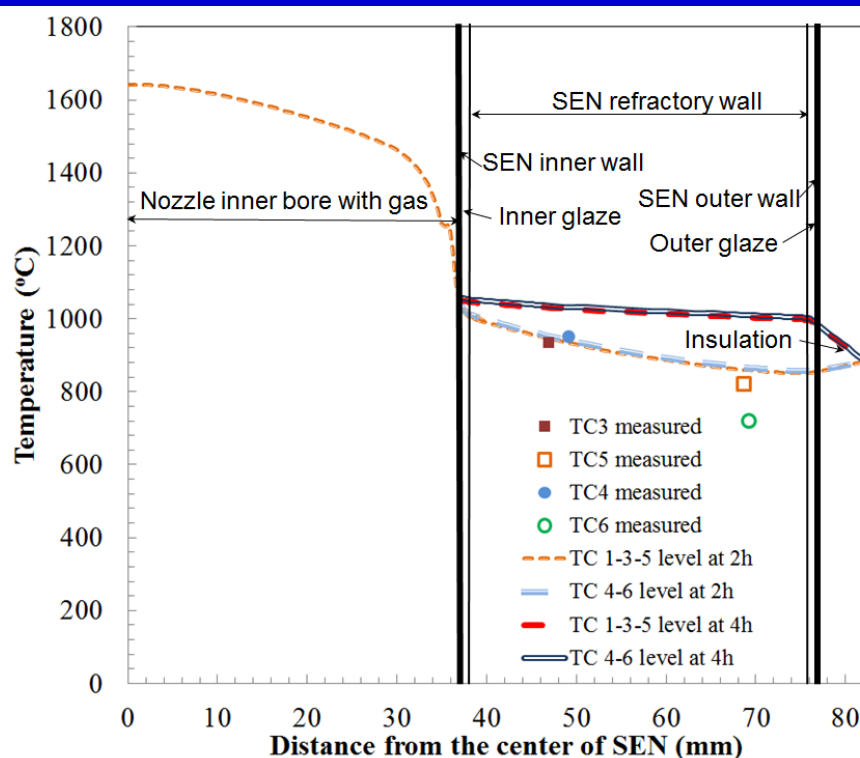
Temperature across SEN: 97mm Validation Case



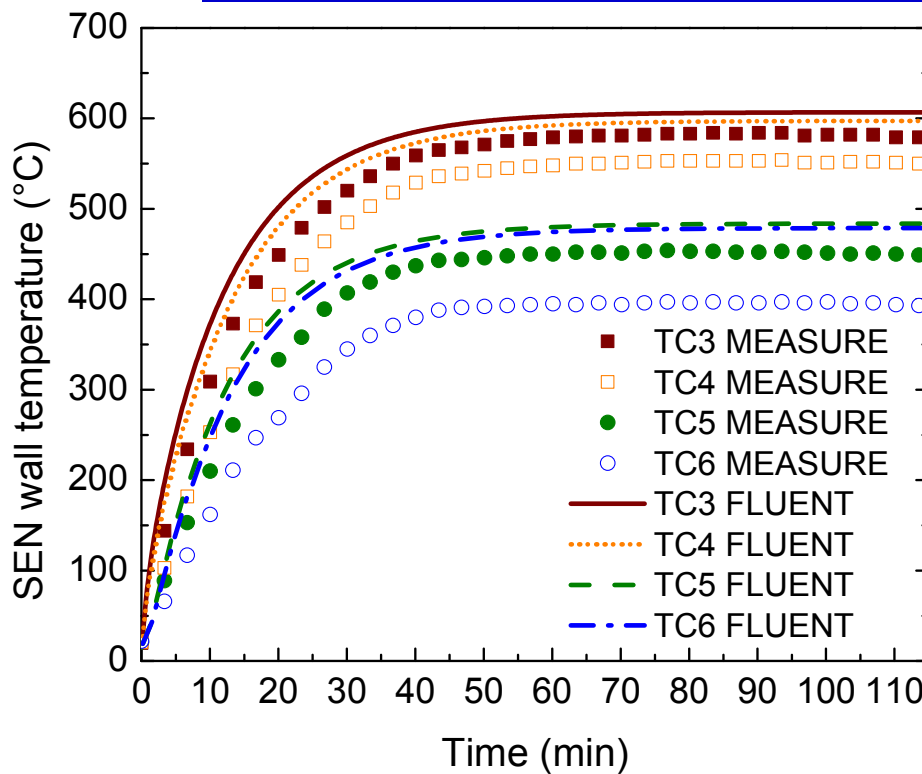
Temperature across SEN: High-k Refractory Case



Temperature across SEN: Insulation Case



Transient temperature validation



TC 3 error= 25°C

TC 4 error= 45°C

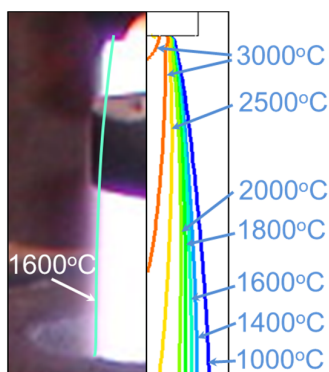
TC 5 error= 32°C

TC 6 error= 83°C

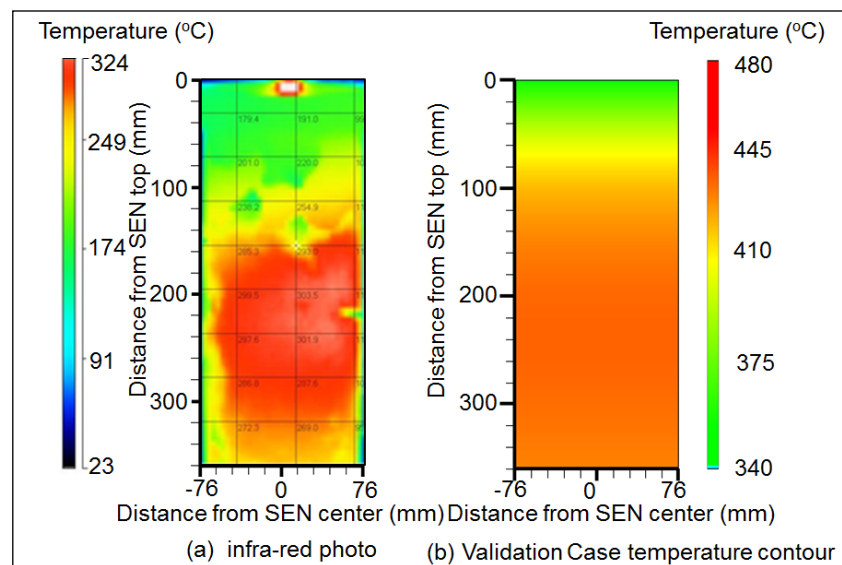
Error causes:

- Excessive thermal conductivity/diffusivity due to uncertain refractory properties
- Neglect of Zirconia sleeve at lower part of SEN
- Neglect of contact resistance at TC tip

Flame shape & Outer wall temperature contour validation



Flame shape comparisons of predicted temperature contours and close-up photograph



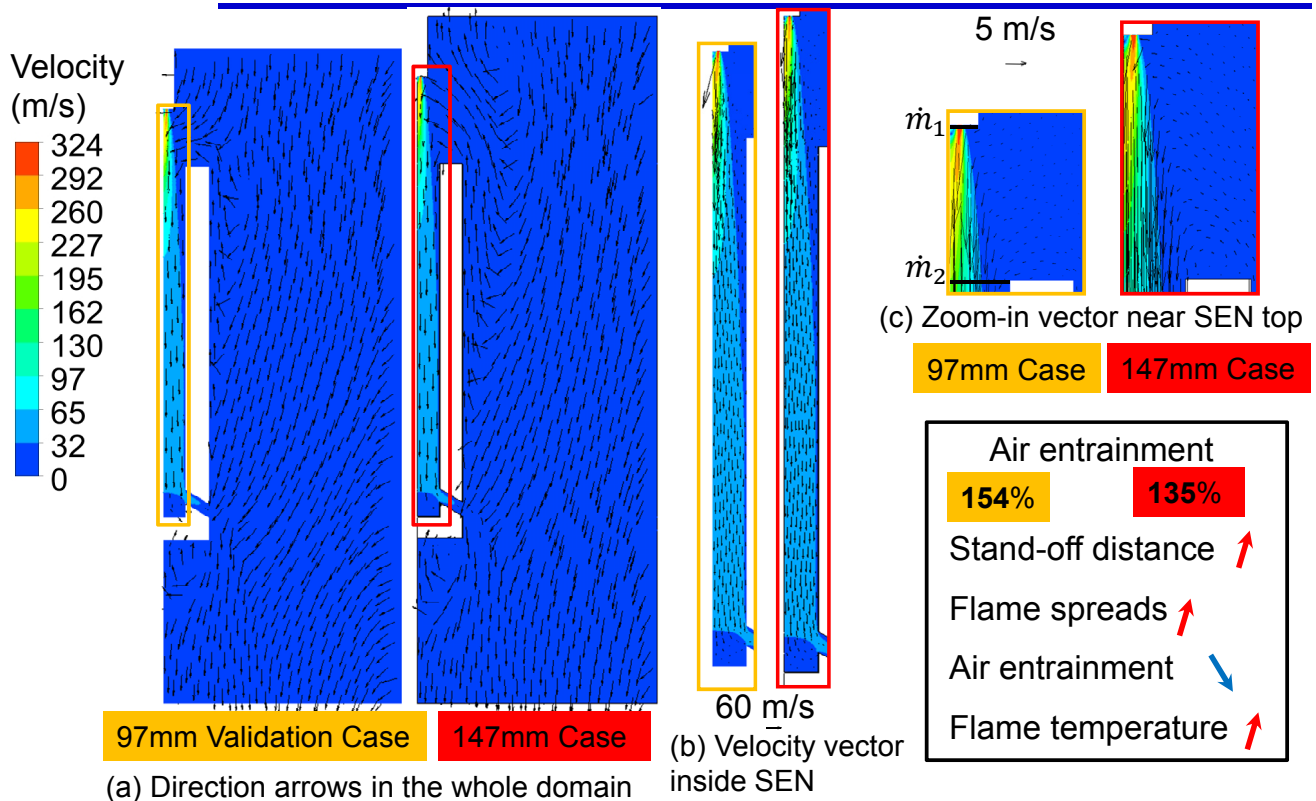
SEN outer wall temperature comparison

Model Parametric study

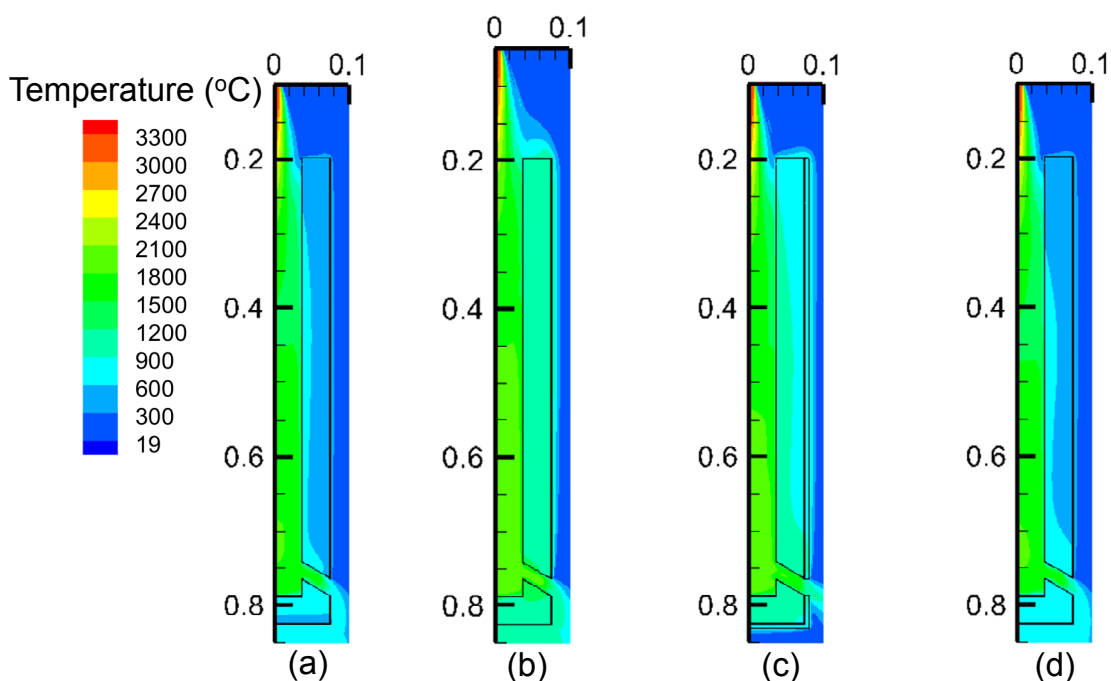
Inputs of 4 cases

Model Inputs	97mm Validation Case	147mm Case	Insulated Case	High-k Case
Thermal conductivity	DG, Glaze	DG, Glaze	DG, Glaze, Insulation	DG, Glaze
Specific heat	DG, Glaze	DG, Glaze	DG, Glaze, Insulation	DG, Glaze
Stand-off distance	97mm	147mm	97mm	97mm
Insulation layer	No	No	Yes	No

Flow distribution



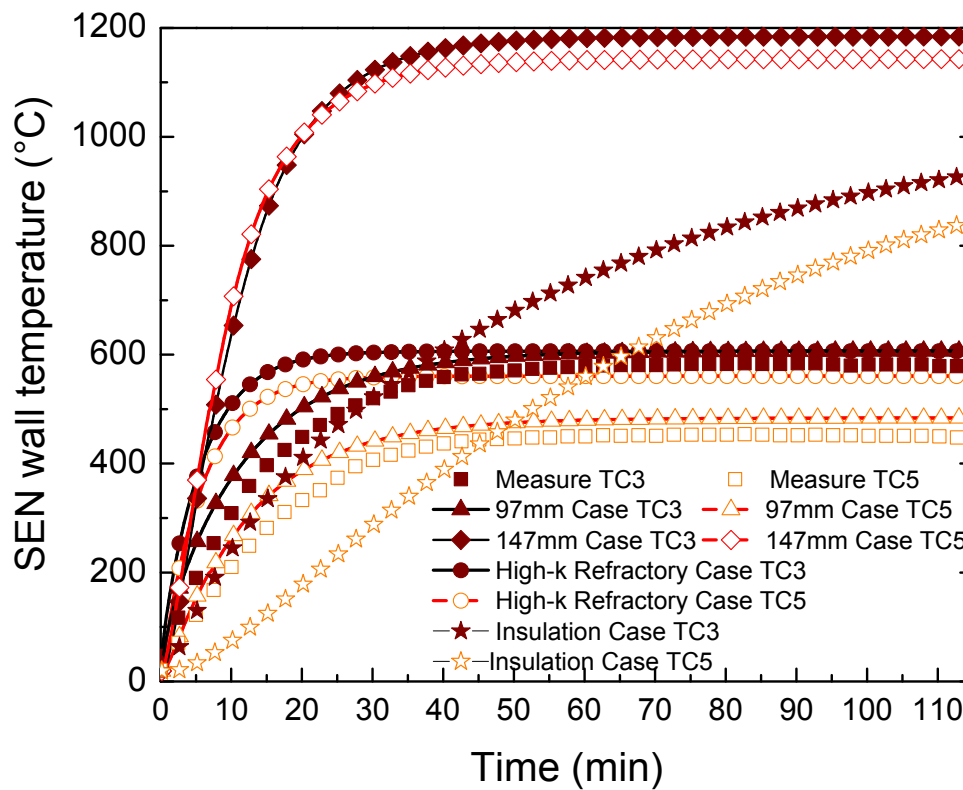
Temperature distribution



(a) 97mm Validation Case
(b) 147mm Case

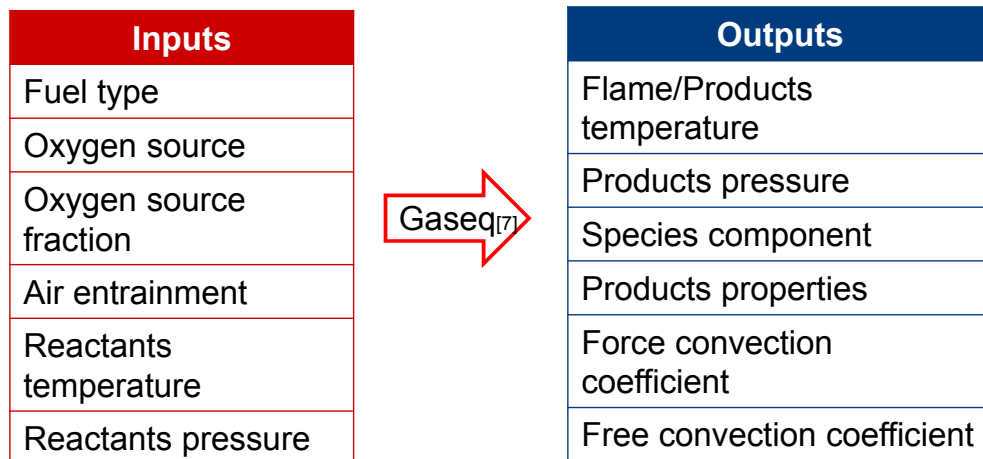
(c) Insulation Case
(d) High-k Refractory Case

Transient temperature comparisons among 4 cases



Flame Temperature Model in Excel VBA

Flame Temperature Model(VBA)



- Gaseq^[7]: a chemical equilibrium program which can predict adiabatic temperature and composition at constant pressure.
- Oxygen Source Fraction = $\frac{\text{mole of oxygen input}}{\text{mole of oxygen required for stoichiometric reaction}}$
- Air Entrainment = $\frac{\text{mole of entrained air}}{\text{mole of air needed for stoichiometric reaction}}$

Flame Temperature Model Results

	Combustion Model	Measurement		Result	Comb. Model
	Air entrainment	Oxygen source fraction	Reactants Temp.	Flame Temp.	Flame temp.
97mm Validation Case	154%	100%	19 °C	1328 °C	1343°C
147mm Case	135%	100%	19 °C	1451 °C	1587°C

Reactants, products pressure is 1atm.

Simple spread-sheet model can predict flame temperature approximately without sophisticated chemical reactions and thermal hydraulic models.

Conclusions

- A **2D axisymmetric** model of nozzle preheating is developed, including **325 chemical reactions with 53 species** of methane combustion.
- **Steady-state** fluid flow, heat transfer and gas combustion, and **transient** heat conduction in the SEN walls are simulated.
- **The model predictions were validated** with a preheating experiment, including the gas temperature across the flame, SEN wall temperature histories, flame shape, and SEN outer wall temperature distribution.
- Moving the burner further away from the SEN top leads to **higher** SEN temperature, due to flame expansion causing less air entrainment.
- Adding **an insulation layer** causes higher SEN wall temperatures and **milder temperature gradients**.
- **Increasing refractory conductivity** causes **milder temperature gradient** at SEN.
- To optimize preheating, a proper stand-off distance, stoichiometric fuel composition, proper refractory thermal properties, and insulation layers are recommended.
- A simple **spread-sheet model** of the adiabatic flame temperature **predicts gas temperature** approximately, based on knowing the **air entrainment**.

Acknowledgements

- The authors are grateful to R. Nunnington and other personnel at Magnesita Refractories for providing the measurement data.
- The authors appreciate the support from the Continuous Casting Consortium at the University of Illinois.

References

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